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Effect of Curing Temperature on the Soil Physical and Mechanical Properties on Clay Shale Geopolymer Fly Ash Stabilization



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Abstract

Clay shale is an easily degraded mudrock when exposed to weathering. The reduced strength due to degradation can be mitigated through soil stabilization. In recent years, soil stabilization using geopolymers has become one of the latest popular methods due to its economic benefits and lower carbon footprint. A widely used cementitious material for this method is fly ash-based geopolymer. The relationship between curing temperatures and the performance of clay shale stabilized with fly ash-based geopolymer has yet to be studied for the purpose of identifying a more effective stabilization method. In this study, clay shale was stabilized using geopolymer. The geopolymer was made of fly ash and an activator. Sodium hydroxide (NaOH) and sodium silicate (Na₂SiO₃) as activators. The activator is diluted with water to create a 12 M mixture. Before the unconfined compressive strength test, the specimens were subjected to various curing temperatures from 26°C to 60°C. The test result shows that, in general, higher curing temperatures increased the dry density from 1.66 g/cm³ to 1.84 g/cm³. While, the unconfined compressive strength multiply about 3.5 times. Furthermore, the the moisture content are decrease after the curing process from 19% to 2.5%. This lead to the specimen volume experiencing decreament due to the shrinkage during the curing veriod. The volume reduce from 67.7 cm³ to 63.5 cm³. In general, temperature plays a significant role in enhancing the strength of clay shale stabilized using fly ash-based geopolymer.

Keywords:

Clay Shale; Curing Temperature; Fly Ash; Unconfined Compressive Strength.

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INTRODUCTION

As a type of mudrock, clay shale is a big problem in construction due to its unstable properties. Clay shale is a 50% to 70% sedimented rock formed mainly by clay minerals, claystone, soil, dust, or rock with cementation [1]. Clay shale is a highly sturdy sedimentation rock. However, clay shale will easily be degraded when exposed to the atmosphere or moistened by water [2]. The degradation altered the geotechnical characteristics and reduced the strength and durability of clay shale [2, 3, 4, 5, 6].

In a construction project, slake deterioration on the surface becomes a major problem in the future when the clay shale is exposed due to the excavation [6]. Alatas et al. [4] reported a landslide event caused by the deterioration process at the Sports Training Center in Hambalang Sentul and on the Semarang-Bawen toll road, precisely, at

Semarang-Bawen toll road KM. 32+000, the clay shale was exposed to the atmosphere due to the slope-cutting works, leading to a collapse on the clay shale slope.

Soil stabilization is widely adopted to improve physical and geotechnical properties. The conventional method is to replace the in-situ soil with material that has suitable properties, such as concrete, or utilize mechanical reinforcement with geogrids or geotextile [7]. Aside from the conventional method, the soil stabilization method arises by mixing the soil with poor engineering properties with cementitious material to improve the soil strength and ductility, reduce swelling potential, permeability, deformation, and settlement, and increase the weathering resistance [1, 2, 8, 9]. The cementitious material will initiate chemical reactions for cation exchange, carbonation, and pozzolanic activity,

thereby enhancing the overall structure of the soil [7, 8].

Recently, geopolymers have become a popular option as an environmentally friendly material for improving soil properties. Murmu et al. [10] utilized a 5M NaOH solution mixed with fly ash geopolymer as a material to stabilize black soil. The results demonstrated that ash-based geopolymer is a viable option for stabilization, particularly in preparing highway subgrade and sub-base. Similar findings were reported by Nguyen and Phan [11], who employed geopolymer for soil stabilization in road construction. Compared to cement, fly ash exhibits a significantly lower global warming potential (GWP), with cement ranging from 0.82 to 0.948 kg CO₂ eq/kg, while fly ash ranges from 0.00526 to 0.027 kg CO₂ eq/kg [10]. Nath et al. [12], reported a 36-43% reduction in carbon footprint by replacing Portland cement with fly ash. Furthermore, fly ash-based geopolymer cement production is reported to have a lower carbon footprint, up to 25% less than that of Portland cement [13].

Fly ash has been utilized as a stabilization material for clay shale, and numerous researchers have studied it with different variables and methods [14, 15, 16]. Sumiyanto et al. [14] employed an injection method to stabilize clay shale using a fly ash-based geopolymer. A mixture of fly ash and alkali was injected into compacted clay shale, resulting in a significant fivefold increase in the unconfined compressive strength of the compacted clay shale. A chemical is needed to activate the fly ash. The activator's type, quantity, and condition are essential in stabilizing the soil. Fly ash with a calcium content <5% (classified as fly ash type F by ASTM) is unable to form a cementitious product [17]. In contrast to type F fly ash, type C fly ash has high amounts of calcium and produces cementitious products [18]. Cristelo et al. [19] used sodium silicate (SiO₂) and sodium hydroxide (NaOH) as activators for type C and F fly ash to stabilize marlstone, which contains high calcium carbonate

Besides fly ash type, other factors such as geopolymer content, molarity, alkali ratio, and curing temperature are significant contributors to the strength of soil stabilized with fly ash-based geopolymer [20]. Hartono et al. [16] investigated the concentration of alkali used as an activator for fly ash-based geopolymer. The study suggests that 12-15M Na₂SiO₃+NaOH concentration is optimal for stabilizing clay shale. However, the correlation between curing temperatures and the performance of clay shale stabilized using fly ash-based geopolymer has not been analyzed. Mapping the interrelation among the influencing

factors can specify a more effective stabilization method. This study will utilize a fly ash-based geopolymer to stabilize clay shale and examine the effect of different curing temperatures on the unconfined compressive strength.

RESEARCH METHOD

Soil Sample

The clay shale used in this study was obtained from the Bawean-Semarang toll road, Central Java. This type of clay shale has a high mechanical property; however, when exposed to water, it quickly degrades. The soil was collected in large boulders and fractured into smaller fragments until passing through sieve No. 4. Figure 1 shows the clay shale used in this study. Smectite clay minerals dominate the soil sample, followed by Illite, Kaolinite, and Chlorite [2]. The soil consists of 93% silt/clay and 7% sand. The grain size distribution of the soil sample is shown in Figure 2. The soil is classified as CH based on the Unified Classification System (USCS), with plastic and liquid limits of 57.9% and 28.4%, respectively. The properties of the soil are presented in Table 1.



Figure 1. The Clay from Bawean-Semarang Toll Road, Central Java

Table 1 Soil Properties of Clay Shale

Soil Properties	Values
Specific gravity, G_s	2.65
Atterberg limits:	
Liquid limit, LL	58%
Plastic limit, PL	28%
Plasticity index, PI	30%
Grand size distribution	
Sand	7%
Silt/Clay	93%
Optimum moisture content, OMC	19%
Maximum dry density, MDD	1.66 (g/cm ³)

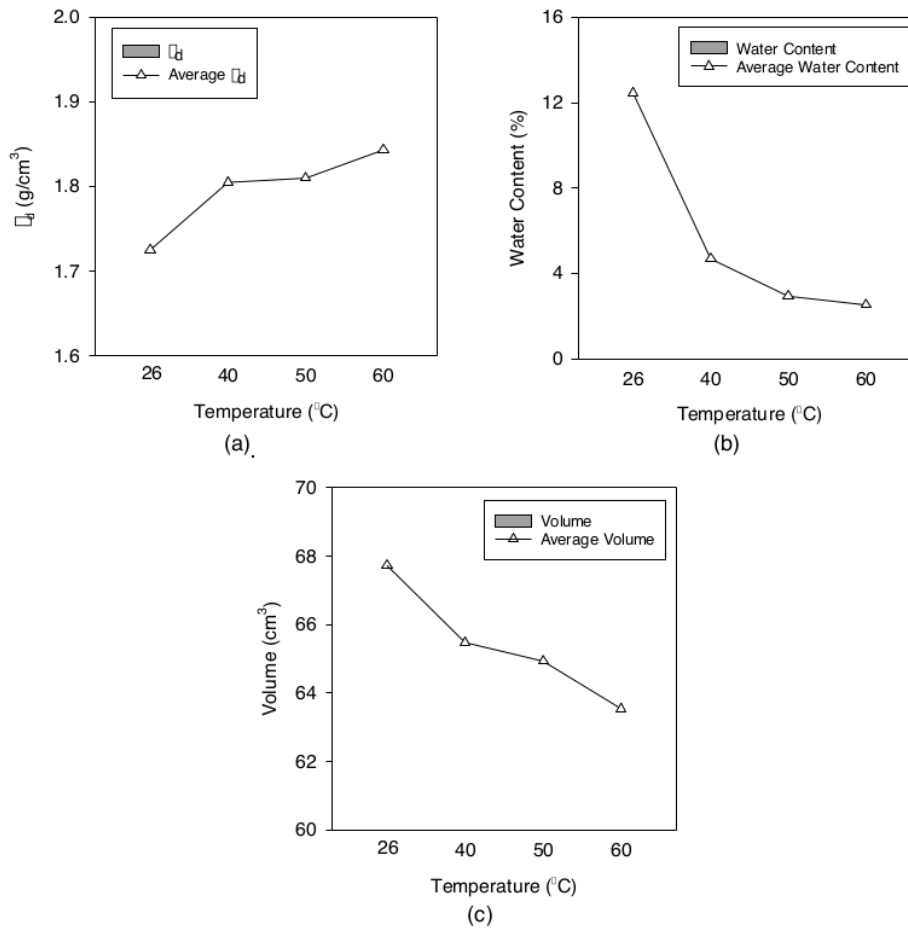


Figure 3 Variation of physical properties of soil stabilized with fly ash-based geopolymer with temperature change (a) dry density, (b) water content (c) volume.

process, leading to specimen shrinkage, thus reducing the volume. The initial average water content of samples is 19% and decreased to 12.5%, 4.7%, 2.9%, and 2.5% for the curing temperatures of 26°C, 40°C, 50°C, and 60°C respectively. Furthermore, the volume are decrease to 67.7 cm³, 65.5 cm³, 64.9 cm³, 63.5 cm³ for 26°C, 40°C, 50°C, and 60°C respectively.

The decrement rate tends to be gentler as the temperature increases. The most significant moisture content drops between 26°C and 40°C are inversely proportional to the dry density results. The average density increased from 1.66 g/cm³ to 1.84 g/cm³. The similar behavior also observed in volume changes where the drastic shrinkage are happen between 26°C and 40°C.

After 40°C, no more significance chance were observed

Effect of temperature on the unconfined compressive strength

Figure 4 shows the stress and strain curves from the UCS test. The UCS test results show almost identical results for each group of samples, with an exception for the samples cured at 50°C. In general, the q_u increases as the curing temperature increases. However, as shown in Figure 4 (c), sample A50-1 has a more rapid increment in the strain for the early loading stage. The peak stress reached 5.8% of strain, the highest value among all specimens. The average q_u is 2.67 MPa, 6.32 MPa, 8.79 MPa, and 9.28

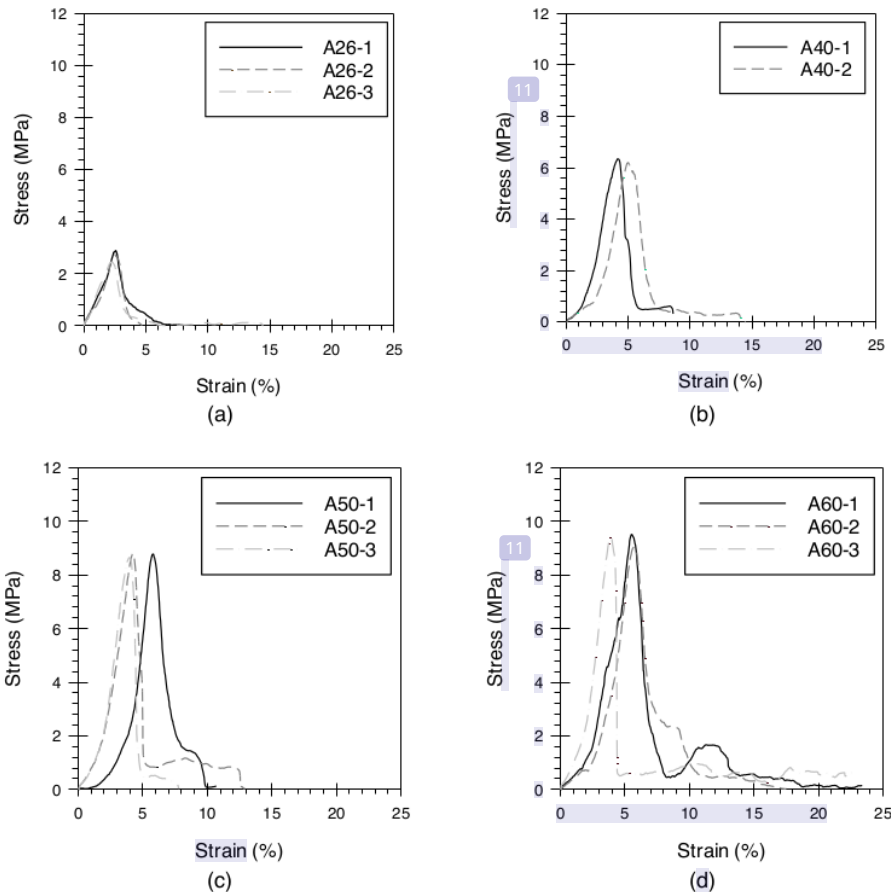


Figure 4 The UCS test result for (a) sample curing at 26°C, (b) sample curing at 40°C, (c) sample curing at 50°C, and (d) sample curing at 60°C.

MPa for specimens A26, A40, A50, and A60. The q_u increases multiply about 3.5 times by increasing the temperature from 26°C to 60°C.

Discussion

As shown in Figure 3, the dry density increased as the curing temperature increased. The increment of soil dry density is related to polymer gel formation, which bonds the soil particles and fills the pores and cracks. It is also possible that the loss of moisture content in the polymerization reaction, which becomes more active in higher temperatures, leads to more rapid moisture loss due to evaporation and causes a volumetric shrinkage [22]. Both polymerization and evaporation cause the sample to become denser.

The process mentioned above is also responsible for the enhancement of mechanical properties. The UCS test results in Figure 4 show that the increment q_u has the same trend as the increment of curing temperature. Leong et al. [23] and Phetchuay et al. [24] mentioned that treating fly ash-based geopolymer in an environment with higher temperatures will lead to a more rapid polymerization reaction in the early stage, resulting in higher early strength. Dissimilar to cement usage as a stabilization material, geopolymers do not form calcium-silicate-hydrates in the soil matrix. Geopolymers utilize an endotherm reaction that absorbs heat from the environment, resulting in polycondensation. Polycondensation is the polymer formation process involving silica and alumina, which leads to the bonding between small molecules and

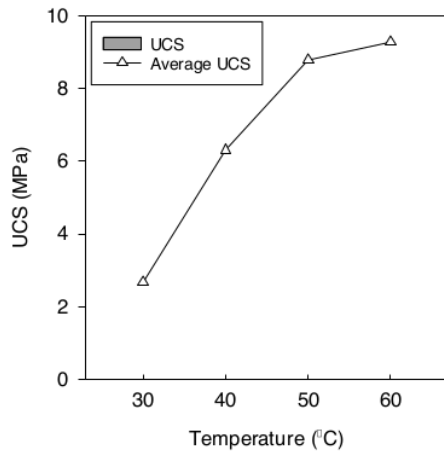


Figure 5 Variation of q_u with temperature

forming alumina-silicate-hydrates. A higher curing temperature and more silica and alumina available to react will lead to more polymerization, thus increasing the number of polymer gels and the bonding strength [25].

The curve shapes are almost identical, with a larger strain at the peak point for samples prepared under different temperatures. However, this trend is negated in samples cured at 50°C. Moreover, specimen A50-1 shows a more considerable deformation before reaching the peak stress, and it fails. Compared to specimen A50-2, specimen A50-1 has a higher dry density, smaller volume, and smaller water content. In this case, the difference in the initial stiffness might be related to the cracks formed during the curing process. Although many cementitious bonds are formed, the rapid moisture loss during curing also makes the sample prone to tension cracks during shrinkage. These cracks were compressed in the initial loading stage, leading to a larger strain. However, the re-structured dried clay shale and the weakened cementitious bonds could still withstand the applied load, even though the additional NaOH do not produce any noticeable positive influence. In addition, the variation in stress-strain behavior might also happen due to the non-optimal mixing process of soil-fly ash-alkali, leading to a non-homogenic mixture.

In general, as summarized in Figure 5, temperature plays a significant role in enhancing the strength of clay shale stabilized using fly ash-based geopolymer. The incrementation of curing temperature shows a stagnancy in the strength development at 50°C or higher. A more rapid polymerization demands more silica and alumina to react. Thus, involving more activators is

required to achieve higher strength. It should be noted that this outcome is the result of an early period of stabilization. The performance of the samples might be different in the later stage after curing (up to 28 days).

CONCLUSION

The study investigates the effect of curing temperature and alkali activator ratio on clay shale stabilization. The unconfined compression test has been successfully conducted. Based on the result and discussion in the earlier section, several notes can be pointed out as follows:

1. The dry density of soil is positively correlated with temperature. There is a significant increase of 0.08 g/cm³ in density between the curing process at ambient temperature (26°C) and 40°C. Nevertheless, the temperature gradually rises until it reaches a curing temperature of 60°C. The test results demonstrate that the highest density in this series of tests is achieved by curing the sample at 60°C.
2. Higher curing temperatures lowered the moisture content after the curing process, leading to specimen shrinkage and thus reducing the volume.
3. The unconfined compressive strength increases as the curing temperature increases. The q_u increases multiply about 3.5 times by increasing the temperature from 26°C to 60°C.

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